

# Rational Approximations Principle for Frequency Shifts Measurement in Frequency Domain Sensors

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**Abstract**—Frequency domain sensors (FDS) are important elements in control, data acquisition and monitoring systems. Such sensors have some outstanding characteristics like output of quasi-digital signals, high sensitivity, high resolution, wide dynamic range, anti-interference capacity and good stability. A FDS converts a physical variable (measurand) into a frequency domain output. When the measurand changes, the output has a proportional frequency shift. In systems that use FDS, measuring the frequency shift is desirable. Accuracy of most frequency measurement techniques is limited by measurement time, and if more precision is required, longer times for measuring are needed. In this work, a novel approach using the rational approximations principle for measuring frequency shift in the output of a FDS is introduced. Also algorithms for simulating the mathematical model of frequency measurement process are proposed, and resolution of measurement is improved by analyzing the data obtained.

**Index Terms**—frequency measurement, frequency shift, FDS

## I. INTRODUCTION

Frequency domain sensors (FDS) are used for measuring physical parameters (measurand). In FDS (also known as “frequency output sensors”), the measurand is converted into a quasi-square wave with a frequency or period [1]. After the measurand variation, a frequency shift occurs in the sensor’s output. Frequency meters are used for measuring the FDS output value.

Quartz crystal microbalances and surface acoustic wave sensors are examples of FDS. When a frequency domain sensor experiments a frequency shift, the variations on its output are several orders of magnitude below the original output value. We’ll briefly review some examples of frequency shifts in FDS reported on the literature. In [2], a silver-coated QCM resonator operating to 9 MHz experimented a frequency shift around 80 Hz, and frequency shifts were recorded by an Agilent 53131A universal counter. A QCM with fundamental frequency of 5 MHz with frequency shifts of 20 Hz was reported in [3], and the measurements were performed using QCM200 Quartz Crystal Microbalance (Stanford Research Systems). 16 MHz QCM with frequency shift close to 20 Hz was reported in [4].

Accuracy of most frequency measurement techniques is limited by measurement time [5], [6]. As consequence if more precision is required, longer times for measuring are needed. A novel technique proposed by Sergiyenko-Hernandez [7] is a powerful tool for fast frequency measurement. Advantages of this method have been explored, such as invariance to jitter [8] and high resolution [9]. Also, diverse applications on automotive [10], [11] and aerospace industries [12], [13] have been proposed. The frequency measurement principle by rational approximations [7] is a suitable tool for analyzing frequency shifts in FDS outputs. Most analysis are made when

the measurand is in steady-state, this means that frequency value has a fixed value. In this work, frequency shift analysis is introduced, and results of analysis are presented and discussed.

## II. FREQUENCY MEASUREMENTS USING THE RATIONAL APPROXIMATIONS PRINCIPLE

In this section, a short review of the frequency measurement principle by rational approximations is introduced. Also the mathematical modeling and parameters of signals required for measuring is presented.

The frequency measurement principle by rational approximations states that, by comparing a signal to be measured ( $S_x$ ), having an unknown frequency ( $f_x$ ) against a reference signal ( $S_0$ ) whose frequency ( $f_0$ ) is known,  $f_x$  can be calculated. In this method, both signals must be conditioned in such way, that the pulse width ( $\tau$ ) in each period in both signals is the same, also  $\tau < T_0$ , where  $T_0$  is the period of  $S_0$ . Pulses in signals after conditioning process are shown on Fig. 1, where  $t_r, t_h, t_f, t_l$ , are falling time, high level time, falling time, and low level time respectively.  $V_h$  is the high level voltage, and  $V_l$  is the low voltage level .

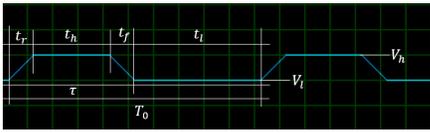


Figure 1. Pulses in signals after signal conditioning

After the previous conditions are fulfilled, the signals are multiplied using the AND-logical function, this leads to the creation of a coincident pulse train ( $S_x \& S_0$  of Fig. 2). When the pulses in both signals exist at the same time, there is a pulse coincidence, if the duration of the coincidence has the same value than  $\tau$ , a perfect coincidence exists, otherwise there is a partial coincidence. As it can be seen on Fig. 1, the pulses in any signal ( $S_x \& S_0$ ) are not perfectly square. The last is due the existence of  $t_r$  and  $t_f$ , as consequence the ideal value of  $\tau$  is  $\tau = t_r + t_f + t_h$ . If  $\tau \gg t_r$  and  $\tau \gg t_f$ , then  $\tau \approx t_h$ . The true value of  $\tau$  is of paramount importance in real systems. In [13], [12], coincidence detectors were proposed. The variations of between  $V_l$  and  $V_h$  affect the duration of  $\tau$ , because the digital circuits used for building a coincidence detector are limited in their input by a low-high logic level. The true value of  $\tau$  is  $t_h < \tau < t_r + t_f + t_h$ .

When two perfect coincidences exist, a mediant fraction is formed, and the condition of Eq. 1 es hold (Fig. 2):

$$\frac{P_{n+i}}{Q_{n+i}} < \frac{P_{n+i} + P_n}{Q_{n+i} + Q_n} < \frac{P_n}{Q_n}, \quad (1)$$

where,  $P_n$  and  $Q_n$  are independent counts of unknown and reference pulses on the considered interval of time (as shown on Fig. 2),  $n$  is the number of fraction and  $i$  is an entire positive number; speaking precisely,  $P_{n+i}$  and  $Q_{n+i}$  appear after one iteration after  $P_n$  and  $Q_n$ , the  $n+i$  value increases as result of time measurement until a number  $m$  where the best

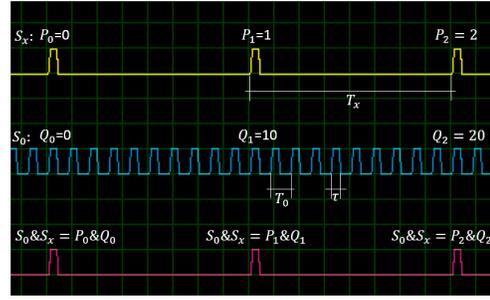


Figure 2. Frequency measurement by rational approximations: signals comparison

approximation is obtained, this is another well known property in classic metrology, by increasing measurement time, the accuracy of measurement increases [14]. Finally the unknown frequency value ( $f_x$ ) of  $S_x$  can be obtained using the known frequency value ( $f_0$ ) of standard  $S_0$ :

$$f_x = f_0 \frac{P_n}{Q_n}, \quad (2)$$

from Eq. 1 and 2:

$$f_x = f_0 \frac{\sum_m P_n}{\sum_m Q_n}. \quad (3)$$

The relative error ( $\beta$ ) for the frequency measurement principle by rational approximations is given by:

$$\beta = \frac{\left| f_x - \frac{P_n}{Q_n} f_0 \right|}{f_x}, \quad (4)$$

and the measurement time ( $M_t$ ) since the beginning of measurement process until the  $n$ -fraction is expressed as:

$$M_t = Q_n T_0 = \frac{Q_n}{f_0}. \quad (5)$$

## III. MEASUREMENT MODEL SIMULATION

The mathematical model exposed in section 2 can be analyzed using computational tools. The model a frequency measurement system using rational approximations has been previously explored, and analyzed trough computational simulations [1], [7], [12], [9], [15]. In the cited papers, just stationary frequency values were analyzed. For the purposes of this work, new simulations algorithms are proposed and implemented in Matlab.

Given the simulation time ( $SimTime$ ) and the period ( $T$ ) of a signal to model, an array of numbers (integers or floating values) is generated using the algorithm 1. In each iteration, the array time keeps an addition of the signal's periods. The number of periods correspond to the number of iterations ( $i$ ). Also in each iteration, the value of  $ElapsedTime$  increments by one value of  $T$ . The array  $Time$  keeps increasing while the  $ElapsedTime$  is lower than  $SimTime$ .

Our interest is to detect when a coincidence occurs. According to Fig. 2, when a coincidence occurs a time of coincidence

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**Algorithm 1** Signal generator

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SIGNAL( $T, SimTime$ )

```
1 ElapsedTime = i = 0
2 while ElapsedTime < SimTime
3   Time[i] = ElapsedTime
4   ElapsedTime = Time[i] + T
5   i ++
6 return Time
```

---

( $t_c$ ) exists. Our analysis indicates that  $0 < t_c \leq \tau$ . The algorithm 2 allow us to get two arrays ( $P, Q$ ), that correspond to the fraction where the coincidence occurred. Algorithm 2 works as follows. In line 1, the variables used for counting are initialized. Unknown frequency and reference signals are generated using algorithm 1 in lines 2 and 3 respectively. Two “while” loops are used for comparing data of each position in  $Signalfo$  and  $Signalfx$ . In line 6 is calculated the time of coincidence. If the condition on line 7 holds, the values of the fraction where the coincidence occurred are recorded.

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**Algorithm 2** Coincidence detector

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COINCIDENCE( $SimTime, \tau, T_x, T_0$ )

```
1 a, b, c = 0
2 Signalfo = SIGNAL( $T_0, SimTime$ )
3 Signalfx = SIGNAL( $T_x, SimTime$ )
4 while a < length(Signalfo)
5   while b < length(Signalfx)
6      $t_c = \tau - |Signalfo[a] - Signalfx[b]|$ 
7     if  $t_c > 0$ 
8        $P[c] = b$ 
9        $Q[c] = a$ 
10      c ++
11     b ++
12    a ++
13 return P, Q
```

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The values of  $P_n, Q_n$  obtained trough algorithm 2 can be used for calculating the value of  $f_x$  (Eq. 3) or relative error (Eq. 4).

In the next section, the presented algorithms are implemented and used for frequency measurement.

#### IV. MEASURING FREQUENCY SHIFTS IN FDS

In a FDS before a measurand change, there is an initial frequency value ( $f_s$ ), and after change a different frequency ( $f_p$ ) value exists. After measurement, the value of  $f_x$  can either approximate to  $f_s$  or  $f_p$ .

A frequency shift ( $\Delta f$ ) is defined as:

$$\Delta f = f_s - f_p. \quad (6)$$

According to Eq. 6, the value of a frequency shift could be obtained by measuring  $f_s$  before, and  $f_p$  after measurand change. From Eq. 6, new operation conditions are needed for frequency meters. If the value of  $f_x$  changes, it will affect the values of  $P_n$  and  $Q_n$  in Eq. 2 and 3. In this section, we

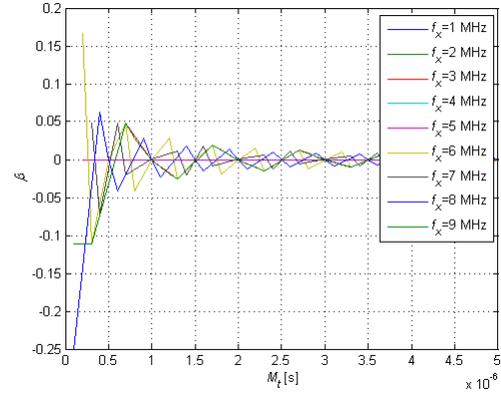


Figure 3. Relative error in frequency measurement process using  $f_0 = 10$  MHz

will discuss the effect of frequency shifts in fast frequency measurement using the rational approximations principle.

##### A. Measurement of $f_s$

In previous works, the rational approximation principle has been used for measurement of steady frequency values [12], [13]. The output of a FDS has an unknown frequency value, such value can be modeled using the previously proposed algorithms. Let us consider  $f_s = f_x$ ,  $f_x = \{1, 2, \dots, 9\}$  MHz,  $\tau = \frac{4}{10}T_0$ , and  $T_0 = 10$  MHz. The frequency measurement process is simulated using algorithm 2, and the relative error of the analyzed values of  $f_x$  is shown on Fig. 3

The relative error ( $\beta$ ) is calculated using Eq. 4. The data obtained from simulations is summarized on Table I. As it is shown in Fig. 3, for all the analyzed values,  $\beta$  has a maximum relative error in the two first fractions. This is due to the first fraction that has  $P_0 = Q_0 = 0$ , and the next fraction is the first approximation. After  $P_1$  and  $Q_1$ ,  $\beta$  decreases while the measurement time is incremented. As it has been shown in previous works, if the principle of rational approximations is used for frequency measurement, the value of  $\beta$  reduces when the measurement time increases (as it can be seen on Table I and using Eq. 5).

Also, a very important property of the rational approximations principle is shown: by increasing the order of  $f_0$  a better approximation to  $f_x$  is obtained. For this case, when  $f_0 = 10$  MHz (Fig. 3), the value of  $f_x$  is approximated in a longer time than when  $f_0 = 100$  MHz (Fig. 4). If  $f_0 = 100$  MHz, the best approximation to  $f_x$  is obtained almost since the start of frequency measurement. The data obtained from simulations is shown on Table 4.

There are cases where  $P_1/Q_1 = f_x/f_0$ , these are known as perfect coincidences. In consequence:

$$\frac{nP_1}{nQ_1} = \frac{f_x}{f_0}, \quad (7)$$

the last will be the best approximations since  $n = 1$ . In Table I, there are perfect coincidences since  $n = 1$  when  $f_x = 1, 2, 4$  and  $5$ . From Table I, a relationship between  $f_x, f_0$  and

Table I  
DATA OBTAINED FROM COMPUTATIONAL EXPERIMENTS WHEN  $f_0 = 10$  MHz

$f_x$ [MHz]	$\frac{P_1}{Q_1}$	$\beta$ in $n = 1$	$\frac{P_m}{Q_m}$	$\beta$ in $m$	$\frac{\sum_m P_n}{\sum_m Q_n}$
1	$\frac{1}{10}$	0	$\frac{9999}{99990}$	0	$\frac{49995000}{499950000}$
2	$\frac{1}{5}$	0	$\frac{19999}{99995}$	0	$\frac{199990000}{999950000}$
3	$\frac{1}{3}$	-0.1111	$\frac{29999}{99997}$	$3.33 \times 10^{-6}$	$\frac{449985000}{1.49995 \times 10^9}$
4	$\frac{2}{5}$	0	$\frac{39998}{99995}$	0	$\frac{399980000}{999950000}$
5	$\frac{1}{2}$	0	$\frac{49999}{99998}$	0	$\frac{1.249975 \times 10^9}{2.49995 \times 10^9}$
6	$\frac{1}{2}$	0.1667	$\frac{59999}{99998}$	$-3.33 \times 10^{-6}$	$\frac{1.79997 \times 10^9}{2.99995 \times 10^9}$
7	$\frac{2}{3}$	0.0476	$\frac{69998}{99997}$	$-1.42 \times 10^{-6}$	$\frac{1.749965 \times 10^9}{2.49995 \times 10^9}$
8	$\frac{1}{1}$	0.2500	$\frac{79999}{99999}$	$2.5 \times 10^{-6}$	$\frac{2.39996 \times 10^9}{2.99995 \times 10^9}$
9	$\frac{1}{1}$	-0.1111	$\frac{89999}{99999}$	$1.11 \times 10^{-6}$	$\frac{3.149955 \times 10^9}{3.49995 \times 10^9}$

Table II  
DATA OBTAINED FROM COMPUTATIONAL EXPERIMENTS WHEN  $f_0 = 100$  MHz

$f_x$ [MHz]	$\frac{P_1}{Q_1}$	$\beta$ in $n = 1$	$\frac{P_m}{Q_m}$	$\beta$ in $m$	$\frac{\sum_m P_n}{\sum_m Q_n}$
1	$\frac{1}{100}$	0	$\frac{9999}{999900}$	0	$\frac{49995000}{4.9995 \times 10^9}$
2	$\frac{1}{50}$	0	$\frac{19999}{999950}$	0	$\frac{199990000}{9.9995 \times 10^9}$
3	$\frac{1}{33}$	-0.0101	$\frac{29999}{999967}$	$3.33 \times 10^{-7}$	$\frac{449985000}{1.49995 \times 10^{10}}$
4	$\frac{1}{25}$	0	$\frac{39999}{999975}$	0	$\frac{799980000}{1.99995 \times 10^{10}}$
5	$\frac{1}{20}$	0	$\frac{49999}{999980}$	0	$\frac{1.249975 \times 10^9}{2.49995 \times 10^{10}}$
6	$\frac{1}{17}$	0.0196	$\frac{59999}{99998}$	$-3.33 \times 10^{-7}$	$\frac{1.79997 \times 10^9}{2.99995 \times 10^{10}}$
7	$\frac{1}{14}$	-0.0204	$\frac{69999}{999986}$	$2.857 \times 10^{-7}$	$\frac{1.749965 \times 10^9}{2.49995 \times 10^9}$
8	$\frac{2}{25}$	0	$\frac{79998}{999975}$	0	$\frac{1.59996 \times 10^9}{1.99995 \times 10^{10}}$
9	$\frac{1}{11}$	-0.1111	$\frac{89999}{999989}$	$1.11 \times 10^{-6}$	$\frac{3.149955 \times 10^9}{3.49995 \times 10^{10}}$

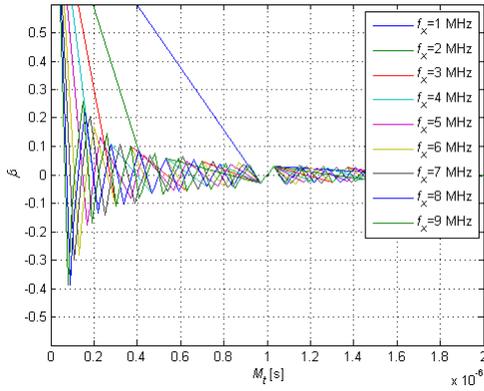


Figure 4. Relative error in frequency measurement process using  $f_0 = 100$  MHz

$\beta$  can be inferred. When the value of  $f_x$  approaches to  $f_0$ , the relative error is incremented. Also  $P_n, Q_n$  start in a value closer to 1, until a best approximation is obtained when  $M_t$  increases. The last observations, lead us to the hypothesis: “if the ratio  $f_0/f_x$  is greater, the value of  $Q_n$  will increase faster. As consequence, the best approximation could be obtained in shorter time”.

In Fig. 4, the results of computational experiments using  $f_0 = 100$  MHz are shown. The other parameters used for simulation still the same used in our previous analysis.

By comparing Fig. 3 and 4, an observation can be done. In the last, the time needed for achieving a better measurement is lower than in Fig. 3. According to Eq. 5, the measurement time decreases when  $f_0$  is increased. In consequence, even if there are the same values of  $P_n$  and  $Q_n$ , the best coincidences will appear in a shorter time. The data shown in Fig. 4 is summarized in Table II.

A comparison of data shown in Table I and II highlights the

importance of the relationship between  $f_x$  and  $f_0$ . In Table II, the value of  $Q_n$  increases faster than in Table I. This is due more pulses of  $S_0$  are counted until the next coincidence appears. Another observation is noted, when the value of  $f_x$  increases, the value of  $P_n/Q_n$  approaches to  $f_x/f_0$  faster. Our analysis is bound to a simulation time (algorithm 1, 2). If the time used for analysis is increases, grater values of  $P_n/Q_n$  would appear and a better approximation to  $f_x/f_0$  could exist. As result, the relative error in frequency measurement decreases. So far, our hypothesis is held and validated by the results of computational experiments.

The resolution of our frequency measurement process is defined by  $n$  and  $f_0$ . When  $n$  increases, more coincidences exist and the value of  $P_n/Q_n$  increases. If  $f_0$  has more orders of magnitude than  $f_x$ , the value of  $Q_n$  increases faster. By comparing Table 4, smaller relative error and better resolution are shown.

Further analysis shows that by increasing the order of  $f_0$ , better approximations in shorter time can be obtained. For practical purposes, there are few constrains. Such as stability of reference standard, and capacity of the circuits used for detecting a pulse width as short as  $\tau < T_0/2$

### B. Measurement of $f_p$

Before we start our analysis, we should make a remark. The frequency measurement principle by rational approximations is based on number theory and deals only with entire numbers [16]. A mediant fraction (Eq. 1) is also known as continuous fraction. The rational approximations are formed by coincidence of pulses, this implies the fact that only complete pulses are counted. Existence of perfect and/or partial coincidences, only depends of the apparition of pulses during a given time.

According to Eq. 6, if  $f_x = f_p$  a frequency shift exists. From our models, the time where the best approximation appears is very short. In order to shown a perceptible change,

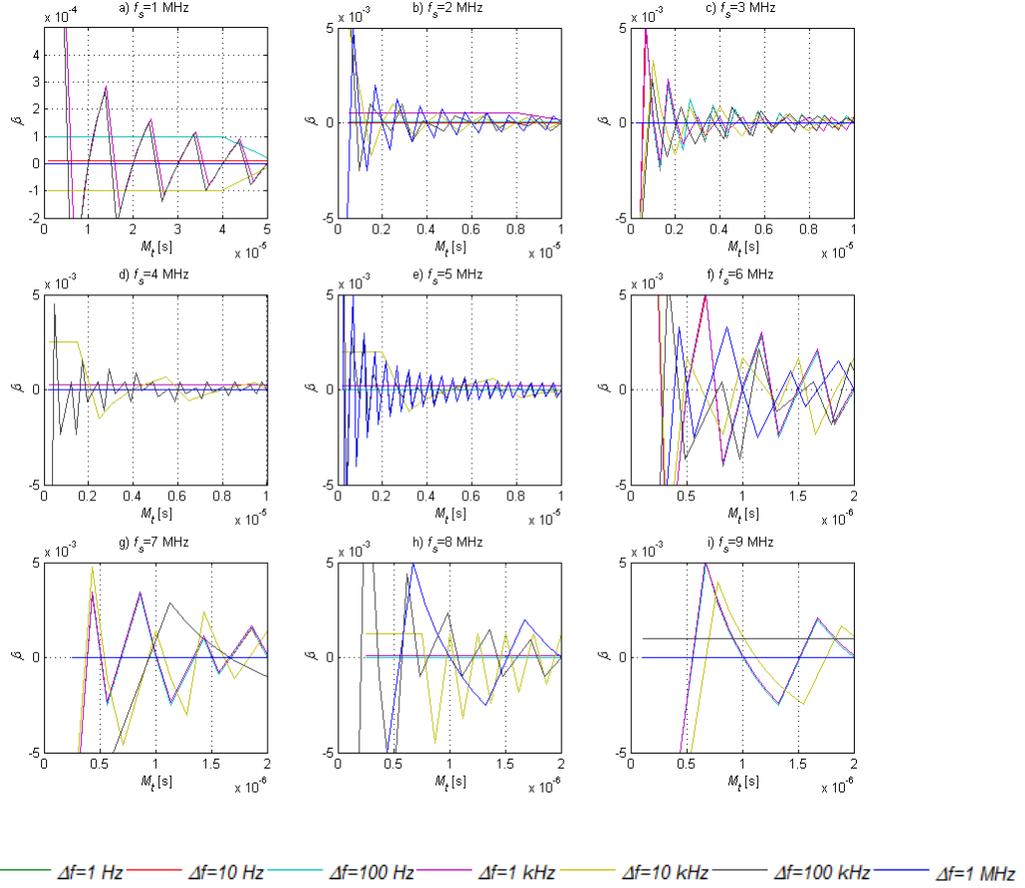


Figure 5. Relative error ( $\beta$ ) during measurement time ( $M_t$ ) in frequency measurement process of  $f_s + \Delta f$ : a)  $f_s = 1$  MHz, b) 2 MHz, c)  $f_s = 3$  MHz, d)  $f_s = 4$  MHz, e)  $f_s = 5$  MHz, f)  $f_s = 6$  MHz, g)  $f_s = 7$  MHz, h)  $f_s = 8$  MHz, i)  $f_s = 9$  MHz.

all the physical variables need a minimum time. Under the idea that our measurement is faster than the speed of change of measurand, the measurement of  $f_p$  can be conceived as stationary state process. From Eq. 3 and 6, the frequency shift can be calculated as:

$$\Delta f = f_0 \frac{\sum_m P_n}{\sum_m Q_n} - f_s \quad (8)$$

Using algorithms 1 and 2 several simulations were carried on. The purpose of such computational experiments was to get clarity about the smallest perceptible  $\Delta f$  that could be measured. The simulations were carried on with  $\Delta f = \{0.1, 1, 100, 1 \times 10^3, 1 \times 10^4, 1 \times 10^5, 1 \times 10^6\}$  Hz,  $f_p = f_x$ ,  $f_x = \{1, 2, \dots, 9\}$  MHz,  $\tau = \frac{4}{10} T_0$ , and  $f_0 = 100$  MHz. The results are shown on Fig. 5.

After enough time, the relative error shown in Fig. 5 has the same behavior of experiments shown in Fig. 3 and Table II. Also in Fig. 5, in order to appreciate the influence of  $\Delta f$  a smaller measurement time is shown.

In particular, the Fig. 5 b,c,d,e have a similar behavior during the same measurement time. If  $\Delta f$  increases, a smaller influence on  $\beta$  occurs. When the value of  $f_x$  approximates

to  $f_0$ ,  $\beta$  decreases very fast (almost since the beginning of measurement process) or last some time to converge to a near zero value. If  $f_x$  and  $f_0$  are close, the number of coincidences is incremented. When  $\Delta f$  decreases,  $\beta$  is less affected, until  $\beta$  is closer as possible to zero. The worst cases are when  $f_s = 1$  MHz and  $f_s = 9$  MHz, this is because  $f_s + \Delta f$  is either very close or very far from to  $f_0$ .

In general, when the value of  $f_x$  approaches to  $f_0$ ,  $\beta$  needs more time for decreasing. Also,  $\Delta f$  is a small approximation of  $f_x$  to  $f_0$ . This allow us to think that such approximation increments the measurement time required for getting the smallest value possible of  $\beta$ . From previous analysis we learned, that if the value of  $f_x$  is close to  $f_0$  a higher error exists. In the data shown in Fig. 5, in some cases small values of  $\beta$  exists in very short time. The last statements, allow us to think it is because a partial coincidence exist where:

$$\Delta f + f_x = f_x + \beta f_x, \quad (9)$$

or:

$$\Delta f \approx \beta f_x. \quad (10)$$

Eq. 10 has sense only when  $n$  has a small value and  $P_1/Q_1 \approx \sum_m P_n / \sum_m Q_n$ . This indicates that  $\beta$  does not decrease. On the other hand, the best approximations are obtained when:

$$P_1/Q_1 \ll \sum_m P_n / \sum_m Q_n \quad (11)$$

or

$$P_1/Q_1 \gg \sum_m P_n / \sum_m Q_n \quad (12)$$

and  $\beta \approx 0$ .

For each case analyzed on Fig. 5, there is an increment in the number of coincidences. This is the result of an increment of the ratio  $P_n/Q_n$ .

Clearly, our computational experiments have shown there is a relationship between  $f_x$ ,  $f_0$ ,  $n$  and  $\Delta f$ . The smallest detectable value of  $\Delta f$  is bounded by Eq. 10.

## V. CONCLUSIONS AND FUTURE WORK

In this work, by using the rational approximations principle, an initial approach to the problem of measuring frequency shifts on FDS has been carried on. We have shown how accuracy of frequency measurements is affected for many factors. Such as variations in the values of  $f_x$ ,  $f_0$  and  $\Delta f$ .

Many analysis were carried on using the proposed algorithms. In the future we hope to study other properties of our measurement method. Also an ongoing work includes a comparison of algorithms 1 and 2 with a real proposed system [12].

One of the principal contributions of this work is that when  $f_0$  is incremented, a higher resolution can be achieved. The limitations for real systems are stability of reference standard, and capacity of the circuits used for detecting a pulse width as short as  $\tau < T_0/2$ .

Finally, a bound for the smallest detectable value of  $\Delta f$  is given by Eq. 10.

As future work, we expect to increase our analysis and improve the resolution of our measurement technique. This, with the aim of detecting smaller values of  $\Delta f$ .

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## REFERENCES

- [1] Daniel Hernandez-Balbuena, Oleg Sergiyenko, Patricia L. A. Rosas-Méndez, Vera Tyrsa, and Moises Rivas-Lopez. Fast method for frequency measurement by rational approximations with application in mechatronics. In Dr. Luigi Cocco, editor, *Modern Metrology Concerns*, chapter 8, pages 201–220. InTech, 2012.
- [2] Mingqing Yang, Junhui He, Mingzhen Hu, Xiaochun Hu, Chunxiao Yan, and Zhenxing Cheng. Synthesis of copper oxide nanoparticles and their sensing property to hydrogen cyanide under varied humidity conditions. *Sensors and Actuators B: Chemical*, 213:59–64, 2015.
- [3] Vivian E Cornelio, Mariele M Pedroso, André S Afonso, João B Fernandes, M Fátima GF da Silva, Ronaldo C Faria, and Paulo C Vieira. New approach for natural products screening by real-time monitoring of hemoglobin hydrolysis using quartz crystal microbalance. *Analytica Chimica Acta*, 2015.
- [4] V Georgieva, M Aleksandrova, P Stefanov, A Grechnikov, V Gadjanova, T Dilova, and Ts Angelov. Study of quartz crystal microbalance no2 sensor coated with sputtered indium tin oxide film. In *Journal of Physics: Conference Series*, volume 558, page 012037. IOP Publishing, 2014.
- [5] Nikolay V. Kirianaki, Sergey Y. Yurish, and Nestor O. Shpak. Methods of dependent count for frequency measurements. *Measurement*, 29(1):31–50, 2001.
- [6] S. Johansson. New frequency counting principle improves resolution. In *Frequency Control Symposium and Exposition, 2005. Proceedings of the 2005 IEEE International*, pages 628–635, Aug 2005.
- [7] Daniel Hernandez Balbuena, Oleg Sergiyenko, Vera Tyrsa, Larisa Burtseva, and Moises Rivas Lopez. Signal frequency measurement by rational approximations. *Measurement*, 42(1):136–144, 2009.
- [8] Oleg Sergiyenko, Daniel Hernandez Balbuena, Vera Tyrsa, Patricia Luz A. Rosas Mendez, Moises Rivas Lopez, Wilmar Hernandez, Mikhail Podrygalo, and Alexander Gurko. Analysis of jitter influence in fast frequency measurements. *Measurement*, 44(7):1229 – 1242, 2011.
- [9] Fabian N. Murrieta-Rico, Paolo Mercorelli, Oleg Yu. Sergiyenko, Vitalii Petranovskii, Daniel Hernandez-Balbuena, and Vera Tyrsa. Mathematical modelling of molecular adsorption in zeolite coated frequency domain sensors. In *Preprints, 8th Vienna International Conference on Mathematical Modelling*. Vienna University of Technology, 2015.
- [10] O.Y. Sergiyenko, D. Hernández Balbuena, V.V. Tyrsa, P.L.A. Rosas Mendez, W. Hernandez, J.I. Nieto Hipolito, O. Starostenko, and M. Rivas Lopez. Automotive FDS resolution improvement by using the principle of rational approximation. *Sensors Journal, IEEE*, 12(5):1112–1121, 2012.
- [11] F.N. Murrieta R, O. Yu Sergiyenko, V.V. Tyrsa, D. Hernández B, and W. Hernandez. Frequency domain automotive sensors: Resolution improvement by novel principle of rational approximation. In *Industrial Technology (ICIT), 2010 IEEE International Conference on*, pages 1313–1318, 2010.
- [12] Fabian N Murrieta-Rico, Daniel Hernandez-Balbuena, Vitalii Petranovskii, Juan Ivan Nieto Hipolito, Alexey Pestryakov, Oleg Sergiyenko, Mayra Molina, and Vyra Tyrsa. Acceleration measurement improvement by application of novel frequency measurement technique for FDS based INS. In *Industrial Electronics (ISIE), 2014 IEEE 23rd International Symposium on*, pages 1920–1925. IEEE, 2014.
- [13] M. Molina, F. Murrieta, O. Yu Sergiyenko, V. Petranovskii, and D. Hernandez-Balbuena. Frequency measurement by principle of rational approximation for aerospace frequency domain mechanical parameter sensors. *Journal Aeronaut Aeronautics*, 2(111):2, 2013.
- [14] David W Allan. Time and frequency(time-domain) characterization, estimation, and prediction of precision clocks and oscillators. *Ultrasonics, Ferroelectrics and Frequency Control, IEEE Transactions on*, 34(6):647–654, 1987.
- [15] Fabian N. Murrieta-Rico, Vitalii Petranovskii, Oleg Yu. Sergiyenko, Daniel Hernandez-Balbuena, Alexey Pestryakov, and Vyra Tyrsa. Frequency domain sensors and frequency measurement techniques. *Applied Mechanics and Materials*, 756:575–584, 2015.
- [16] GL Litvinov, A Ya Rodionov, and AV Tchourkin. Approximate rational arithmetics and arbitrary precision computations for universal algorithms. *Int. J. Pure Appl. Math*, 45(2):193–204, 2008.